

Effect of addition ZrO₂-Al₂O₃ nanoparticles mixture on some properties and denture base adaptation of heat cured acrylic resin denture base material

Ali MA Aljafery, B.D.S. ⁽¹⁾

Basima MAH, B.D.S., M.Sc., Ph.D. ⁽²⁾

ABSTRACT

Background: The PMMA polymer denture base materials are low mechanical properties, adaptation of the denture base to underlying tissue is important for retention and stability of denture. The aim of the study was to evaluate the effect of mixture ZrO₂-Al₂O₃ nanoparticles on impact strength, transverse strength, hardness, roughness, denture base adaptation of heat cured acrylic resin denture base material.

Materials and methods: One hundred (100) specimens were prepared, the specimens were divided into five groups (20 specimens to each) according to the test type, each group was subdivided into two subgroups (control and experimental) each subgroup consist of 10 specimens, the experimental group included mixture of 2% (ZrO₂-Al₂O₃ ratio 2:1) by weight. The impact strength was measured by Charpy's impact testing machine, the transverse strength was measured by Instron testing machine while the hardness was measured by shore D durometer and roughness was measured by Profilometer. Denture base adaptation was measured by digital microscope and evaluated by computerized tomography (CT).

Results: Highly significant increase of impact and transverse strength, non-significant increase of hardness, significant increase of roughness and reduction of denture base adaptation (measured at 3 point A, B and C) occurred in experimental group when compared to control group. CT evaluation, gap between the denture base and master cast (control and experimental groups) increased from the anterior to posterior side of palate and from the alveolar ridge to the mid palatal line.

Conclusion: The polymer nanocomposites had mechanical properties higher than neat PMMA at same time less denture base adaptation.

Keywords: Acrylic denture base, nano fillers, mechanical properties, denture base adaptation. (J Bagh Coll Dentistry 2015; 27(3):15-21).

INTRODUCTION

Acrylic resin polymethyl methacrylate (PMMA) is the most extensively used material in fabrication of dentures. Although it is very popular, this material is still insufficient in fulfilling the ideal mechanical requirements of such appliances ⁽¹⁾. Clinicians still encounter fracture of this material due to low resistance to impact, flexural, or fatigue stresses ⁽²⁾. In order to prevent fracture of the dentures, the thickness of acrylic resin in susceptible regions, such as the palatal midline, and the mandibular lingual and labial frenal attachments has been increased ⁽³⁾.

In addition, improvement on mechanical properties of denture base materials were tried to be achieved either by adding a polyfunctional cross-linking agent such as polyethylene glycol dimethacrylate ⁽⁴⁾ or by incorporating a rubber phase ⁽⁵⁾, metal oxides, metal wire ^(6,7) or fiber ⁽⁸⁾. The reinforcement of polymers used in dentistry with metal-composite systems has been a prime interest. Addition various amounts of powdered Cu, Ag and Al into the PMMA resin and reported increased compressive strength but decreased tensile strength ⁽⁹⁾.

(1) M.Sc. Student, Department of Prosthodontics, College of Dentistry, University of Baghdad.

(2) Assistant Professor, Department of Prosthodontics, College of Dentistry, University of Baghdad.

Evaluation the changes in the mechanical properties of PMMA, polyethyl methacrylate (PEMA) and poly isobutyl methacrylate (PIMA) resin matrices by reinforcing with oxides of Al, Mg, Zr and pulverized E-glass particles ⁽¹⁰⁾. They suggested that 2% admixtures by volume in PMMA resin matrix resulted in better mechanical properties. Much attention has been directed toward the incorporation inorganic nanoparticles into PMMA to improve its properties. The properties of polymer nanocomposites depend on the type of incorporating nanoparticles, their size and shape, as well as the concentration and interaction with the polymer matrix ⁽¹¹⁾.

Nanoparticles were undergone surface treatment with silane coupling agent and embedded into PMMA ⁽¹²⁾. Alumina nanoparticles were treated with trimethoxysilylpropylmethacrylate (TMSPM) to get PMMA/alumina Nano composite with improved properties over pure PMMA ⁽¹³⁾. Also, using modified ZrO₂ with trimethoxysilylpropylmethacrylate to get PMMA/ ZrO₂ Nano composite to improve properties of PMMA ⁽¹⁴⁾. Furthermore, studying an experimental investigation of mixture HA/AL₂O₃ nanoparticles on mechanical properties of restoration materials ⁽¹⁵⁾. Also, evaluation of influence of mixture of ZrO₂-TiO₂ on mechanical and physical properties

of heat-cured polymethyl methacrylate denture base resins⁽¹⁶⁾. Though the incorporation of fillers like rubber and fibers to heat-cured poly methyl methacrylate resin improves the impact strength and fatigue resistance, it may affect some of the properties of heat-cured poly methyl methacrylate resin such as fitness accuracy (denture adaptation), dimensional stability and the effect of water sorption⁽¹⁷⁾. Various investigators have compared the dimensional changes between

different denture base materials^(17,18), palatal vault configurations⁽¹⁹⁾, methods of packing⁽¹⁸⁾, modes of polymerization⁽²⁰⁾ and curing cycles⁽²¹⁾. This study was conducted to use inorganic mixture of $ZrO_2-Al_2O_3$ Nano fillers that were added to heat cure PMMA and test the effect of this addition on the some mechanical properties and denture base adaptation of heat cured acrylic denture base material.

MATERIALS AND METHODS

Some of the materials used in this study are summarized in table (1).

Table 1: List of the materials that were used

Material	ZrO ₂ nanofiller	Al ₂ O ₃ nanofiller	Trimethoxysilylpropyl methacrylate(TMSPM)	Heat-curing acrylic resin
Manufacturer	HWNANO China	NS6130 01-123 Germany	2530-85-8 Germany	Vertex Netherlands

Test specimens preparation

Two different plastic patterns were constructed according to the required test. The pattern that was constructed for impact strength a bar shaped specimen (80mm X 10mm X 4mm) length, width, thickness respectively⁽²²⁾. For transverse strength test: a bar shaped specimen was constructed (65mm X 10mm X 2.5mm) length, width, thickness respectively⁽²³⁾ (Figure 1). Same specimen measurement was used to prepare hardness test and roughness test. For denture base adaptation test: prepare acrylic resin denture bases with their corresponding master casts by conventional denture flasking technique using a Biostar sheet as record base (2mm thickness) without teeth.

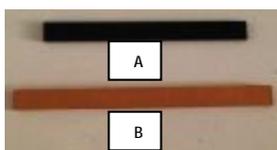


Figure 1: Plastic patterns; A for transverse strength, B for impact strength

Surface modification of nanofillers (ZrO₂, Al₂O₃)

The introduction of reactive groups to the fillers surface was achieved by reaction of 3-trimethoxy silylpropyl methacrylate (TMSPM) with zirconium oxide and aluminum oxide Nano fillers through salinization procedure⁽²⁴⁾. For ZrO₂, TMSPM was used in 5% wt. of nanofiller, toluene was used as a solvent to ZrO₂^(12,14,24), while Al₂O₃, TMSPM was used in 75% wt. of Al₂O₃, ethanol was used as a solvent to Al₂O₃⁽¹³⁾.

Mould preparation

Addition of fillers

This only for experimental group included mixture of 2% (ZrO₂-Al₂O₃ ratio 2:1) by weight, electronic balance (Sartorius, Germany) with sensitivity of (0.0001g) was used to weigh then nanofillers powder weight in 2% wt. of the PMMA powder weight. The filler was added to the monomer of PMMA mixed by the probe sonifier apparatus (DANBURY, U.S.A.) for 3 minutes^(13,14) to disperse the nanoparticles in the monomer and reduce the possibility of particle aggregation.

Mixing of the acrylic

Acrylic material was mixed and manipulated according to manufacturer's instructions using a conventional water bath denture flasking technique for both groups (control and experimental). For experimental group the suspension of the monomer with nanofiller was immediately mixed with acrylic powder.

Mechanical and denture base adaptation tests

1-Impact strength test.

a- All the prepared specimens (20 specimens, 10 for each control and experimental groups) stored in distilled water inside incubator at 37°C for 48 hours before testing⁽²³⁾.

b- Testing procedure: The impact strength test was carried out following the procedure recommended by the ISO 179 using impact testing device (Tmi, testing machine Inc. Amity Ville, New York, USA)⁽²²⁾ (Figure 2). The specimen was supported horizontally at each end and strucked by free swinging pendulum of 2 Joules.

The scale readings give the impact energy in Joules. The Charpy impact strength of un-notched specimen was calculated in Kilo-joules per square meter using the following formula:

Impact strength (kJ/m^2) = $\frac{E}{b \cdot d} \times 10^3$ where E: The impact energy in Joules, b: Is the width of the specimens in millimeters, d: Is the depth of the specimens in millimeters.

2-Transverse strength test.

a. All the prepared specimens (20 specimens, 10 for each control and experimental groups) stored in distilled water inside incubator at 37°C for 48 hours before being tested⁽²³⁾.



Figure 2: Impact strength testing device

3- Measuring hardness property

a- All the prepared specimens (20 specimens, 10 for each control and experimental groups) stored in distilled water inside incubator at 37°C for 48 hours before being tested⁽²³⁾.

b- Testing procedure: Test was performed using durometer hardness tester (shore D hardness, TH210, Italy) which is suitable for acrylic material⁽²³⁾. The instrument consists of a blunt pointed indenter (0.8 mm in diameter) that present in a cylinder (1.6mm in diameter). The indenter was attached to a digital scale that is graduated from 0 to 100 unit. The usual method was to press down firmly and quickly on the indenter, a measurements were taken directly from the digital scale reading. Five measurements were recorded on different areas of each specimen and an average of these five readings was recorded.

4-Measuring surface roughness.

a- All the prepared specimens (20 specimens, 10 for each control and experimental groups) stored in distilled water inside incubator at 37°C for 48 hours before being tested⁽²³⁾.

b- Testing procedure: The Profilometer device surface roughness tester (TH 210, China) was used to test the micro geometry of the surface for experimental and control group. The device has surface analyzer (sharp stylus made from diamond) to trace the profile of the surface irregularities. It moves for maximum distance of 11 mm. The Profilometer records by its scale all

b. Testing procedure: The test was performed using Instron universal testing machine (WDW-200 E, UK) (Figure 3), each specimen was positioned on the bending fixture which consist of two parallel supports (50 mm apart). The load was applied by a rod placed centrally between the supports with across head speed of 1mm/min applied making deflection until fracture occurs. The transverse strength was calculated using the following formula:

Transverse strength (N/mm^2) = $\frac{3PL}{2bd^2}$ Where P: is the peak load, L: is the span length, b: is the sample width, d: is the sample thickness⁽²⁵⁾.



Figure 3: Instron testing device

the peaks and recesses which characterized the surface of the specimen under testing. The analyzer pass along the specimen surface for 11 mm distance. Three locations were selected in every specimen making 3 readings then the mean of these readings were recorded as a surface roughness value for each specimen.

5- Denture base adaptation testing

a- Microscopic measurement: The cast- denture base sets (20 specimens, 10 for each control and experimental groups) was sectioned to a horizontal line 5 mm away from the posterior end of the cast using a cutting saw device under water cooling^(26,27). Three points were marked on the cast on transverse line at the posterior border of the cast specimens (deepest point of the left vestibule, left ridge crest and midline point which is marked according to the line bisecting the incisive papilla and extending posterior on the cast) as (A, B and C) respectively (figure 4)⁽²⁶⁾.

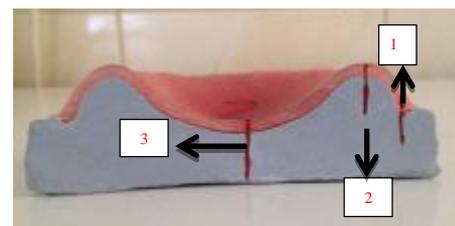


Figure 4: Denture base with its cast show position of 3 points: (1) point A, (2) point B and (3) point C

The gap between the cast and the denture base margin at these 3 points was measured with the use of digital microscope (Dino- Lite, Taiwan) of magnification 200x capability and accuracy of 0.001 mm. Two measurements were made, first one made immediately after deflasking and sectioning for all the samples. Second measurement was done after incubation in distilled water at 37°C for 14 days for all the samples⁽²⁷⁾, then each denture base was seated on its corresponding cast and measurement of the

gab was done while a weight of 1kg was placed over the denture base to ensure a proper seating of the denture base over the cast⁽²⁶⁾.

b- To observe the overall gap formation of the denture base, All denture bases placed on their respective master cast for each group was scanned by computerized tomography (Light Speed, Philips, Netherland), (figure 5). The frontally-sectioned images of the denture-cast set and sagittal images obtained at the palatal midline were taken from the CT data⁽²⁷⁾.



Figure 5: A- computerized tomography device, B- The casts with their corresponding denture bases under scanning

RESULTS

Mean values, standard deviation, t-test, p-value and Significances of mechanical properties presented in table (2).

Table 2: Descriptive and statistics of mechanical properties

Property	Tested groups	N	Mean	S.D.	T-test	P. value	Sig.
Impact strength (Kj/m ²)	Control group	10	7.94	0.25	-16.02	0.000	HS
	Experimental group	10	9.63	0.22			
Transverse strength (N/mm ²)	Control group	10	88.50	0.77	-11.85	0.000	HS
	Experimental group	10	93.48	1.08			
Surface hardness	Control group	10	84.64	1.12	-1.316	0.205	NS
	Experimental group	10	85.35	1.27			
Surface roughness (µm)	Control group	10	1.29	0.08	-2.309	0.033	S
	Experimental group	10	1.37	0.07			

Mean values, standard deviation, t-test, p-value and Significances of the gap at three selected points (A, B and C) to measure denture base adaptation presented in table (3).

Table 2: Descriptive and statistics of the gap(mm)at three point

point	Time	Tested groups	N	Mean	S.D.	T-test	P-value	Sig.
Point A	Immediately After deflasking	Control group	10	0.122	0.018	-2.160	0.045	S
		Experimental group	10	0.160	0.054			
	After incubation 14 day	Control group	10	0.143	0.038	-2.266	0.036	S
		Experimental group	10	0.195	0.063			
Point B	Immediately After deflasking	Control group	10	0.065	0.016	-2.61	0.018	S
		Experimental group	10	0.081	0.013			
	After incubation 14 day	Control group	10	0.088	0.035	-1.64	0.111	NS
		Experimental group	10	0.113	0.036			
Point C	Immediately After deflasking	Control group	10	0.244	0.040	-0.711	0.486	NS
		Experimental group	10	0.257	0.033			
	After incubation 14 day	Control group	10	0.284	0.053	-0.524	0.607	NS
		Experimental group	10	0.301	0.087			

Evaluation of denture base adaptation made by CT images (Figure 6) was at the mid sagittal line of denture bases on the respective master cast for all tested specimen (control and experimental groups), gap formation between the tissue surface of the denture base and master cast increased from

the anterior to posterior side of palate and also from the alveolar ridge to the mid palatal line. However, the gap distance or volume could not be measured from the CT images due to the low resolution.

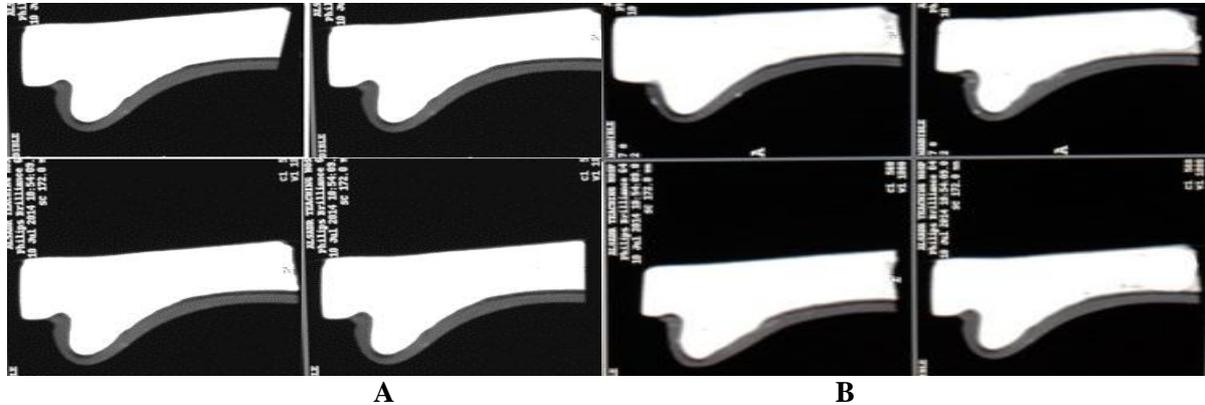


Figure 6: Computerized tomography images for denture-cast sets: A. control group, B. experimental group

DISCUSSION

The present study was conducted to evaluate and compare the effect of addition ($ZrO_2:Al_2O_3$ nano-fillers mixture) to PMMA on some mechanical properties and denture base adaptation of heat cured acrylic denture base. The introduction of nanofillers into PMMA produced highly significant increase in the value of impact strength when compared with control group. The increase in the impact strength could be due to the high interfacial shear strength between nanofiller and matrix resulted from the formation of cross-links or supra molecular bonding which cover or shield the Nano fillers which in turn prevent propagation of cracks. Also the crack propagation may be changed by good bonding between nanofiller and resin matrix resulted from interaction between the functional groups introduced by salinization process⁽²⁸⁾. The small size and high surface area and relatively low concentration may helped in a good distribution of these fillers that may cause a restricted motion of macromolecule chains and enhance mechanical properties⁽²⁹⁾, that means the PMMA nanocomposite has mechanical stability more than neat PMMA.

Also, the transverse strength test result showed highly significant increase with nanocomposite when compared with control group. This increase in transverse strength may be explained on the basis of transformation toughening, when sufficient stress develops and crack begins to propagate, a transformation of ZrO_2 and Al_2O_3 which depletes the energy of crack propagation,

also, in this process expansion of ZrO_2 and Al_2O_3 crystals occurs and places the crack under a state of compressive stress and crack propagation is arrested⁽²⁵⁾.

Increase in transverse strength also could be due to transfer of stress from more flexible polymer to the higher modulus, more rigid and stiffer filler particles⁽²⁵⁾. The addition of nanofillers at 2wt.% to PMMA led to increase of surface hardness beyond that of pure PMMA, statistically was not-significant, this could be due to the relatively low concentration of the nanofillers used in the study, although, this improvement may be attributed to the inherent characteristics of the nanoparticles. Nanoparticles possess strong ionic interatomic bonding, giving rise to its desirable material characteristics, that is, hardness and strength. On these bases it may be expected when nanoparticles disperse in a matrix, they increase its hardness and strength⁽³⁰⁾.

The surface roughness of modified PMMA with nanofiller was significantly increased when compared with control group. This is may be due to the difference in roughness of Nano particles and acrylic denture base matrix and also probably attributed to the difference in micro structural characteristics of the materials and the form of the particles⁽³¹⁾.

With regard to this study, the significantly increase in surface roughness can be considered uninfluential since microorganism colonization occurs when the roughness more than $0.2\mu m$ ⁽³²⁾. The gap between denture base and cast was measured at 3 point (A, B, C) in two time to

evaluate denture base adaptation, where it mostly depend on polymerization shrinkage and water sorption of PMMA^(33,34). So, in first measurement made immediately after deflasking showed a significant increase of gap in experimental group when compared to control group at point A and B, and non-significant increase of gap in experimental group at point C. This increase explained may be due to addition of nanoparticle lead to increase in thermal conductivity of acrylic resin^(13,30), and degree of polymerization effected considerably by heat dissipation and thermal conductivity⁽³⁵⁾, lead to contraction of denture base due to further polymerization shrinkage that occur due to exposure to high temperature with reduction in the spaces between the chain of the polymer this result in agreement with Ogawa and Hasegawa⁽³⁶⁾.

In second time after incubation 14 day showed in a significant increase of gap in experimental group when compared to control group at point A, and non-significant increase of gap in experimental group at point B and C. This result may be due to that the addition of nanoparticles to PMMA may decreased in water sorption when compared with unmodified PMMA^(13,16), So decrease expansion of acrylic denture base which considered antagonist effect to polymerization shrinkage that occur in experimental group more than control group as discussed previously⁽³⁷⁾.

The CT images of denture base-cast sets did show this tendency of gap formation in medial-lateral and anterior-posterior areas (Figure 6). These findings are also predictable with the results reported by Consani et al.⁽³⁸⁾, who compared the posterior border gap of the denture base-cast sets sectioned transversally at each area of the canine, molar and posterior ends. Moreover, the magnitude of the posterior border gap generally increased medially along the palatal vault reaching a maximum at the midline of the palate^(39,40).

REFERENCES

1. Darbar UR, Huggett R, Harrison A. Denture fracture-a survey. *Br Dent J* 1994; 176: 342-5.
2. Jagger DC, Harrison A, Jandt KD. Review: The reinforcement of dentures. *J Oral Rehabil* 1999; 26:185-94.
3. Meng TR Jr, Latta MA. Physical properties of four acrylic denture base resins. *J Contemp Dent Pract* 2005; 6: 93-100.
4. Kanie T, Fujii K, Arikawa H, Inoue K. Flexural properties and impact strength of denture base polymer reinforced with woven glass fibers. *Dental Materials* 2000; 16: 150-8.
5. Knott NJ. The durability of acrylic complete denture bases in practice. *Quintessence Int* 1989; 20: 341-3.
6. Ruffino AR. Effect of steel strengtheners on fracture resistance of the acrylic resin complete denture base. *J Prosthet Dent* 1985; 54: 75-8.
7. Teraoka F, Nakagawa M, Takahashi J. Adaptation of acrylic dentures reinforced with metal wire. *J Oral Rehabil* 2001 28; 937-42.
8. Goldberg AJ, Burstone CJ. The use of continuous fiber reinforcement in dentistry. *Dent Mater* 1992; 8: 197-202.
9. Sehajpal SB, Sood VK. Effect of metal fillers on some physical properties of acrylic resin. *J Prosthet Dent* 1989; 61: 746-51.
10. Zuccari AG, Oshida Y, Moore BK. Reinforcement of acrylic resins for provisional fixed restorations. Part I: Mechanical properties. *Biomed Mater Eng* 1997; 7: 327-43.
11. Jordan J, Jacob KL, Tannenbaum R, Shart MA, Jasiuk I. Experimental trends in polymer Nanocomposites-A review. *Mater Sci Eng* 2005; 393(1) 1-11.
12. Shi J, Bao Y, Huang Z, Weng Z. Preparation of PMMA-Nanometer calcium carbonate composites by in-situ emulsion polymerization. *J Zhejiang University Sci* 2004; 5(6) 709-13.
13. Jasim BS. The effect of silanized alumina Nano fillers addition on some physical and mechanical properties of heat cured polymethyl methacrylate denture base material. M.Sc. Thesis, College of dentistry/University of Baghdad, 2013.
14. Safi IN. Evaluation the effect of modified Nano filler addition on some properties of the heat cure acrylic risen denture base material. M.Sc. thesis, College of Dentistry, University of Baghdad, 2011.
15. Majid S, Nabi MK, Abbas R. An experimental investigation of HA/AL2O3 nanoparticles on mechanical properties of restoration materials. *Engineering Solid Mechanics* 2014; 2:173-82.
16. Asar NV, Hamdi A, Turan K, Ilser T. Influence of various metal oxides on mechanical and physical properties of heat-cured polymethylmethacrylate denture base resins. *J Adv Prosthodont* 2013; 5: 241-7.
17. Becker CM, Smith DE, Nicholls J. The comparisons of denture base processing technique. II. Dimensional changes due to processing. *J Prosthet Dent* 1977; 37: 450-90.
18. Anusavice KJ. *Phillip's science of dental material*. 10th ed. Philadelphia: W.B, Saunders Co.; 1996. p. 211, 220, 235, 237-271.
19. Craig RG, O'Brien WJ, Powers JM. *Dental-materials properties and manipulation*. 4th ed. St. Louis: CV Mosby Co.; 1990. p. 272-96.
20. Anderson GC, Schulte JK, Arnold TG. Dimensional stability of injection and conventional processing of denture base acrylic resin. *J Prosthet Dent* 1988; 60(3): 394-8.
21. Chen JC, Lacefield WR and Castleberry DJ. Effect of denture thickness and curing cycle on the dimensional stability of acrylic resin denture bases. *Dent Mater J* 1988; 4: 20-4.
22. ISO 179-1 International organization for standardization. Determination of Charpy impact properties: Part 1, 2000.
23. American Dental Association Specification No.12. Guide to dental materials and devices. 10th ed. Chicago, 1999; p: 32.
24. Ayad NM, Badawi M, Abdou A Fatah. Effect of reinforcement of high-impact acrylic resin with

- zirconia on some physical and mechanical properties. Rev Clinical Dental 2008; 4(3): 145-51.
25. Anusavice KJ. Philips science of dental material. 11th ed. Middle East and African ed., Ch7, Ch22, 2008; p: 143-166,721-756.
 26. Hussein YA. Influence of different pH of saliva and thermal cycling on the adaptation of different denture base materials. M.Sc. Thesis, College of Dentistry/ University of Baghdad, 2012.
 27. Lee C, Bok S, Bae J, Hae-hyoung Lee. Comparative adaptation accuracy of acrylic denture bases evaluated by two different methods. Dent Mater J 2010; 29(4): 411-7.
 28. Sun L, Gibson RF, Gordaninejad F, Suhr J. Energy absorption capability of nanocomposites: a review. Composites Science and Technology 2009; 69(14): 2392-409.
 29. Gupta N, Brar BS, Woldesenbet E. Effect of filler addition on the compressive and impact properties of glass fiber reinforced epoxy. Bull Mater Sci 2001; 24:219-23.
 30. Ellakwa AE, Morsy MA, El-Sheikh AM. Effect of aluminum oxide addition on the flexural strength and thermal diffusivity of heat-polymerized acrylic resin. J Prosthodont 2008; 17: 439-44.
 31. Alnamel HA. The effect of silicon dioxide nano-fillers reinforcement on some properties of heat cure poly methacrylate denture base material. M.Sc. thesis, College of Dentistry, University of Baghdad, 2013.
 32. Quirynen M, Marechal M, Busscher HJ, Weerkamp AH, Darius PL, Steerberghe D. The influence of surface free energy and surface roughness on early plaque formation: an in vivo study in man. J Clin Periodontol 1990; 17:138-44.
 33. Wolfoardt J, Cleaton-Jones P, Fatti P. The influence of processing variables on dimensional changes of heat cured poly methyl methacrylate. J Prost Dent 1986; 55: 518-25.
 34. Salim S, Sadamori S, Hamada T. The dimensional accuracy of rectangular acrylic resin specimens cured by three denture base processing methods. J Prosthet Dent 1992; 67: 879-81.
 35. Dhuru VB. Contemporary dental materials. Oxford University UK, 2003.
 36. Ogawa T, Hasegawa A. Effect of curing environment on mechanical properties and polymerizing behavior of methyl- methacrylate auto polymerizing resin. J Oral Rehabil 2005; 32: 221-6.
 37. Andrew J. Polymer chemistry properties and application. Carlverlag publisher, 2006; Ch. 23 p. 339-45.
 38. Consani RL, Domitti SS, Consani S. Effect of a new tension system, used in acrylic resin flasking, on the dimensional stability of denture bases. J Prosthet Dent 2002; 88: 285-9.
 39. Laughlin A, David Eick J, Alan G, Leslie Y, Dorsy J. A comparison of palatal adaptation in acrylic denture bases using conventional and anchored polymerization techniques. J Prosthodont 2001; 10(4): 204-11.
 40. Takamata T, Setcos JC, Phillips RW, Boone ME. Adaptation of acrylic resin dentures as influenced by the activation mode of polymerization. J Am Dent Assoc 1989; 119: 271- 6.

الخلاصة

خلفية: مادة قاعدة الطقم البوليميثيلميثاكريليت (الراتنج الأكريليك) البوليمر ذات خواص ميكانيكية منخفضة، وتكيف قاعدة الطقم إلى الأنسجة الكامنة مهم لاستبقاء واستقرار قاعدة الطقم. وكان الهدف من هذه الدراسة هو تقييم تأثير خليط الحبيبات النانوية لأوكسيد الألمنيوم وأوكسيد الزركونيوم على قوة الصدمة والقوة العرضية، صلابة و خشونة السطح، وتكيف قاعدة الطقم لمادة قاعده طقم الراتنج الأكريليك الحراري.

المواد والطرق: أعدت مائة عينة، تم تقسيم هذه العينات إلى خمس مجموعات (عشر وعينة لكل مجموعة) وفقاً لنوع الاختبار، ومن ثم تم تقسيم كل مجموعة إلى مجموعتين (السيطرة والتجريبية) كل مجموعة فرعية تتكون من عشرة عينات، وتضمنت المجموعة التجريبية خليط من 2٪ وزناً ل (أوكسيد الزركونيوم وأوكسيد الألمنيوم) من مسحوق البوليميثيلميثاكريليت، ونسبة (1:2:1) $ZrO_2:Al_2O_3$. تم قياس قوة الصدمة بواسطة آلة اختبار الصدمة (Charpy)، تم قياس القوة العرضية بواسطة آلة اختبار إنسترون (INSTRON) بينما تم قياس صلابة السطح بواسطة مقياس (Shore D durometer)، وتم قياس خشونة السطح من قبل Profilometer. تم قياس تكيف قاعدة الطقم بواسطة المجهر الرقمي وتقييمها من قبل جهاز التصوير المقطعي المحوسب (CT).

النتائج: زيادة كبيرة للغاية في قوة الصدمة والقوة العرضية، وزيادة غير كبيرة في الصلابة، وزيادة كبيرة في الخشونة ونقصان تكيف قاعدة الطقم الذي تم قياسه عند ثلاث (3) نقاط هي (A، B، C) حصلت في المجموعة التجريبية مقارنة بالمجموعة السيطرة. أما تقييم جهاز التصوير المقطعي المحوسب، الفجوة بين قاعدة الطقم والقالب الرئيسي لكلا المجموعتين (السيطرة والتجريبية) يظهر فيه زيادة من الجانب الأمامي إلى الخلفي من سقف الحلق ومن قمة عظم الفك إلى خط منتصف الحنك.

الاستنتاج: مادة النانو المركبة على أساس البوليمر لديها خواص ميكانيكية أعلى من الراتنج الأكريليك البوليمر الحراري النقي وفي نفس الوقت نقصان في تكيف قاعدة الطقم.

الكلمات الرئيسية: قاعدة طقم الأكريليك، خشونة النانو، الخواص الميكانيكية، وتكيف قاعدة الطقم.